

# APPLICATION NOTE

## ***On-Line Estimation of Grass Reference Evapotranspiration with the Campbell Scientific Automated Weather Station***



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With increasing pressure on water supplies and concerns over the groundwater contamination which results from overirrigation, it is becoming increasingly important to know how much water crops need. This information is most useful if it is supplied in real-time as the water loss occurs. Fortunately, modern dataloggers and sensors are capable of making the measurements and computations necessary to provide this information. This application note describes the computations necessary for estimating grass reference evapotranspiration ( $ET_0$ ). The reference crop is defined as a short grass crop that is not short of water.

A number of methods have been used to estimate grass reference evapotranspiration. Many are reviewed and evaluated by Jensen et al. (1990). The most successful are combination methods that use measurements of absorbed radiant energy, wind, and atmospheric vapor deficit. A number of studies have shown that the Penman-Monteith form of the combination equation consistently outperforms the others. This equation includes more of the factors that influence crop water loss than the other equations, and is therefore expected to provide better estimates. It has not been used in the past in operational applications because of its additional computational complexity and the need to define standard values for the reference crop. Past grass reference  $ET_0$  computations have usually been made using daily, rather than hourly data. More empirical equations, which were derived using daily average data, might be expected to work better under these conditions. However, with the capabilities of microprocessor-based dataloggers to do on-line computations, many limitations have been removed, and the more physically sound Penman-Monteith equation has become feasible for operational applications.

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## The Penman-Monteith Equation

The Penman-Monteith (PM) equation can be written as:

$$ET_o = \frac{\Delta(R_n - G)}{\lambda(\Delta + \gamma^*)} + \frac{\gamma^* M_w (e_a - e_d)}{R \Theta r_v (\Delta + \gamma^*)} \quad (1)$$

$ET_o$	Potential evaporation ( $\text{kg m}^{-2} \text{ s}^{-1}$ or $\text{mm s}^{-1}$ )
$R_n$	Net radiation ( $\text{kW m}^{-2}$ )
$G$	Soil heat flux density ( $\text{kW m}^{-2}$ )
$M_w$	Molecular mass of water ( $0.018 \text{ Kg mol}^{-1}$ )
$R$	Gas constant ( $8.31 \times 10^{-3} \text{ kJ mol}^{-1} \text{ K}^{-1}$ )
$\Theta$	Kelvin temperature (293 K)
$e_a - e_d$	Vapor pressure deficit of the air (kPa)
$\lambda$	Latent heat of vaporization of water ( $2450 \text{ kJ kg}^{-1}$ )
$r_v$	Canopy plus boundary layer resistance for vapor ( $\text{s m}^{-1}$ )
$\Delta$	Slope of the saturation vapor pressure function ( $\text{Pa } ^\circ\text{C}^{-1}$ )
$\gamma^*$	Apparent psychrometer constant ( $\text{Pa } ^\circ\text{C}^{-1}$ )

Details on the derivation of this equation can be found in Monteith and Unsworth (1990) and Campbell (1977). The Automated Weather Station measures air temperature, relative humidity, incident solar radiation, and wind speed. A number of conversions and assumptions is needed to convert these measurements to the parameters for the PM equation. We will generally follow the recommendations suggested by Smith (1991), since these have been recommended as standards for use throughout the world by the Food and Agriculture Organization of the United Nations.

The net radiation is the sum of the net solar radiation and the net long-wave radiation. This is approximated as:

$$R_n = a_s S_t + L_{ni} \quad (2)$$

Where  $a_s$  is the absorptivity of the crop for solar radiation,  $S_t$  is the incident solar radiation measured by the datalogger, and  $L_{ni}$  is the atmospheric radiant emittance minus the crop emittance at air temperature. Monteith and Unsworth (1990) show that, under clear skies,  $L_{ni}$  is closely approximated by:

$$L_{nic} = 0.0003 T_a - 0.107 \text{ (kW m}^{-2}\text{)} \quad (3)$$

where  $T_a$  is the air temperature in degrees Celsius ( $^{\circ}\text{C}$ ). Under cloudy skies,  $L_{ni}$  increases and approaches zero. We estimate cloudiness from the ratio of measured to potential solar irradiance during daylight hours:  $S_t/S_o$ . A cloudiness function is then computed as:

$$f(S_t/S_o) = 1 - 1/[1+0.034 \exp (7.9 S_t/S_o)] \quad (4)$$

The net isothermal long-wave for cloudy skies can then be calculated by multiplying the value obtained from the cloudy function with the approximation of the long-wave radiation for clear skies:

$$L_{ni} = f(S_t/S_o) L_{nic} \quad (5)$$

Equation 4 requires the computation of  $S_o$ , the potential solar radiation on a horizontal surface outside the earth's atmosphere. This is calculated from:

$$S_o = 1.36 \sin \phi \quad (6)$$

where  $1.36 \text{ kW m}^{-2}$  is the solar constant, and  $\phi$  is the elevation angle of the sun.  $\sin \phi$  is computed from:

$$\sin \phi = \sin d \sin l + \cos d \cos l \cos [15(t-t_o)] \quad (7)$$

where  $d$  is the solar declination angle,  $l$  is the latitude of the site,  $t$  is clock time, and  $t_o$  is the time of solar noon. The declination angle is often evaluated using several terms of a Fourier series, but, since Campbell Scientific dataloggers are particularly adept at evaluating polynomials, we chose to approximate  $\sin d$  using the following polynomial:

$$\sin d = -0.37726 - 0.10564j + 1.2458j^2 - 0.75478j^3 + 0.13627j^4 - 0.00572j^5 \quad (8)$$

where  $j$  is (day of the year)/100. The cosine is computed from the trigonometric identity:

$$\cos d = (1 - \sin^2 d)^{1/2} \quad (9)$$

For running the PM algorithm, we assume the user always sets the clock to standard time (not daylight savings time). The time,  $t$ , needed for Eq. 7 is therefore just the datalogger clock time less half the time increment from the last  $ET_o$  computation. The time of solar noon is given by:

$$t_o = 12.5 - L_c - t_e(\text{hr}) \quad (10)$$

where  $L_c$  is a longitude correction and  $t_e$  is the “Equation of Time.” The longitude correction is a user-supplied parameter. It is calculated by determining the difference between the longitude of the site and the longitude of the standard meridian. Standard meridians are at  $0^\circ$ ,  $15^\circ$ ,  $30^\circ$ .. $345^\circ$ . Generally time zones run approximately  $\pm 7.5^\circ$  on either side of a standard meridian, but this varies depending on political boundaries (see Figure 1). The user should check an atlas to get both the longitude and the standard meridian for the site (as well as the latitude, which is also needed for Eq. 7). The longitude correction is computed from:

$$L_c = (L_s - L)/15. \quad (11)$$

If the longitude of the site were  $L=117^\circ$ , and the longitude of the standard meridian were  $L_s=120^\circ$ ,  $L_c$  would be  $(120-117)/15 = 0.2$  hr. If the longitude of the site were  $123^\circ$ ,  $L_c$  would be  $-0.2$  hr.

The Equation of Time is an additional correction to the time of solar noon that depends on day of the year. Again, we used a polynomial for the computation. Two equations were used, one for the first half of the year, the other for the second half. For the first half (day of year  $\leq 180$ ),

$$t_e = -0.04056 - 0.74503j + 0.08823j^2 + 2.0516j^3 - 1.8111j^4 + 0.42832j^5, \quad (12)$$

where  $j = (\text{day of the year})/100$ . For day of the year  $> 180$ ,

$$t_e = -0.05039 - 0.33954j + 0.04084j^2 + 1.8928j^3 - 1.7619j^4 + 0.4224j^5, \quad (13)$$

where  $j = (\text{day of the year} - 180)/100$ .

Latitude must also be taken into account. For latitudes above the equator, the value used will be positive. Below the equator, the value for latitude will be negative.

Evapotranspiration occurs mainly during daytime hours when net radiation is positive. When  $R_n$  is positive, the soil heat flux density can be reliably estimated as a fraction of  $R_n$ . For complete canopy cover (the condition specified for reference  $ET_o$ ), we can use:

$$G = 0.1 R_n \quad (14)$$

When  $S_t = 0$  (night), we can use  $G = 0.5 R_n$  or  $G = 0.5 L_{ni}$ .

The variable,  $\Delta$ , is the slope of the saturation vapor pressure function, and depends only on air temperature. We use a polynomial to evaluate  $\Delta$ :

$$\Delta = 45.3 + 2.97 T + 0.0549 T^2 + 0.00223 T^3 \quad (\text{Pa } ^\circ\text{C}^{-1}) \quad (15)$$

for the temperature range of  $-5^\circ$  to  $45^\circ\text{C}$ .

The apparent psychrometer constant,  $\gamma^*$ , is calculated from:

$$\gamma^* = \gamma r_v/r_a \quad (16)$$

where  $\gamma$  is the thermodynamic psychrometer constant,  $r_v$  is the combined canopy and aerodynamic resistance to water vapor, and  $r_a$  is the convective resistance for heat transfer. The vapor resistance is computed from  $r_v = r_a + r_c$  where  $r_c$  is the canopy resistance. Smith (1991) gives, as standard for a reference crop,  $r_c = 70 \text{ s m}^{-1}$ . At night, the stomatal resistance increases so the value of  $700 \text{ s m}^{-1}$  is assigned to  $r_c$  when solar power drops below  $10 \text{ W m}^{-2}$ . He also gives the relationship,  $r_a = 209/u_2$ , where  $u_2$  is the wind speed measured at a height of 2 m above the ground. For wind measured at 3 m height ( $u_3$ ), the relationship is  $r_a = 240/u_3$ . These values are a simple reduction of the equation:

$$r_a = \ln\left[\frac{z_u-d}{z_{om}}\right] \ln\left[\frac{z_t-d}{z_{oh}}\right] / k^2 u_{zu} \quad (17)$$

where  $k = 0.41$ ,  $z_u$  is the height of the anemometer above the soil surface and  $z_t$  is the height of the hygrometer (temperature and RH) above the soil surface. If  $d$  is  $0.67 H$  and  $z_{om}$  is  $0.12 H$  for clipped grass with  $z_{oh} = 0.1 z_{om}$  (Allen et al., 1989 and ASCE 70), then, for  $0.12 \text{ m}$  grass,  $r_a = 209/u_2$  for a  $2 \text{ m}$  anemometer, RH and temperature height and  $r_a = 240/u_3$  for a  $3 \text{ m}$  anemometer, RH, and temperature height.

The thermodynamic psychrometer constant has a weak temperature dependence, which we ignore, and a pressure dependence, which we account for. At sea level and  $20^\circ\text{C}$ ,  $\gamma = 67.3 \text{ Pa}$ . The value decreases in direct proportion to atmospheric pressure, so we multiplied this value by the ratio of atmospheric pressure to sea level pressure, which we calculated from the altitude of the site:

$$P/P_o = \exp(-A/8500) \quad \text{or} \quad P/P_o = \exp(-B/27889) \quad (18)$$

where A is the altitude in meters or B is the altitude in feet.  
Altitude is another value that the user must supply.

The Kelvin temperature in the denominator of Eq. 1 was set at 293 K, so that the combination,  $M_w/R\Theta$ , could be pre-computed and entered as a constant in the program. While this has a small temperature dependence, it is certainly negligible compared to the other uncertainties in Eq. 1.

Vapor pressures in Eq. 1 are computed from the air temperature and relative humidity measurements. The saturation vapor pressure at air temperature,  $e_a$ , is obtained from the datalogger saturation vapor pressure function, with air temperature as the argument. The saturation vapor pressure at dew point temperature,  $e_d$ , (or air vapor pressure) is obtained from  $e_d = h_r e_a$ , where  $h_r$  is the relative humidity (as a fraction, not a percent).

## Implementing the Penman Monteith Calculation in the CR10X

The attached program example implements the PM calculation in our CR10X. There are a number of comments which show how the equations are implemented. The calculations are done in subroutine 1. The user-supplied information is shown in steps 2, 3, and 4 of Table 3. The wind speed factor is set for a height of 3 m. If the anemometer is at a different height, this value should be changed in step 67 of Table 3.

Weather variables are sampled every 10 s; hourly values for grass reference crop  $ET_o$  ( $E_p$ ) are computed from the sampled data hourly. The hourly values are stored in final memory and also summed to give a daily value. The time of day for output is set in steps 56, 62, and 70 in Table 1, so the daily sums are from the time set on one day to that same time on the next. Normally this would be set at midnight (1440), but an irrigation manager might want an earlier readout time so that night time irrigation could be planned at the end of each day.

Users of this program should be aware of its limitations. We feel that it represents the best available method for computing grass reference crop evapotranspiration. However, crops differ in their water requirements. The ET of a crop depends on several factors in addition to  $ET_o$ , including stage of development, crop height, ground cover, etc. Engineers account for these factors by using a

crop coefficient to multiply  $ET_o$ . For a complete cover of short grass, the crop coefficient is 1. Contact Campbell Scientific Environmental Application Engineering Department for a list of crop coefficients and a discussion of their use.

Another important consideration is the quality of the input data. No matter how good the algorithm, if the measurements are faulty, the predictions will be useless. The user needs to make sure that the latitude, longitude correction, and altitude supplied to the program are correct, and that the datalogger clock is set to correct standard time. If these values are wrong, the estimates of the long-wave radiation will be wrong. It is also important to use a regular schedule of maintenance and recalibration assuring the sensors operate correctly. For example, if the wind speed sensor were to malfunction and give a wind speed reading of zero,  $\gamma^*$  would become infinite, and the algorithm would predict zero  $ET_o$ , regardless of the actual  $ET_o$ . As the algorithms become more sophisticated and accurate, the need for accurate environmental data increases. Calibration on anemometers, pyranometers, and humidity sensors should be checked at least annually against standards.

#### References

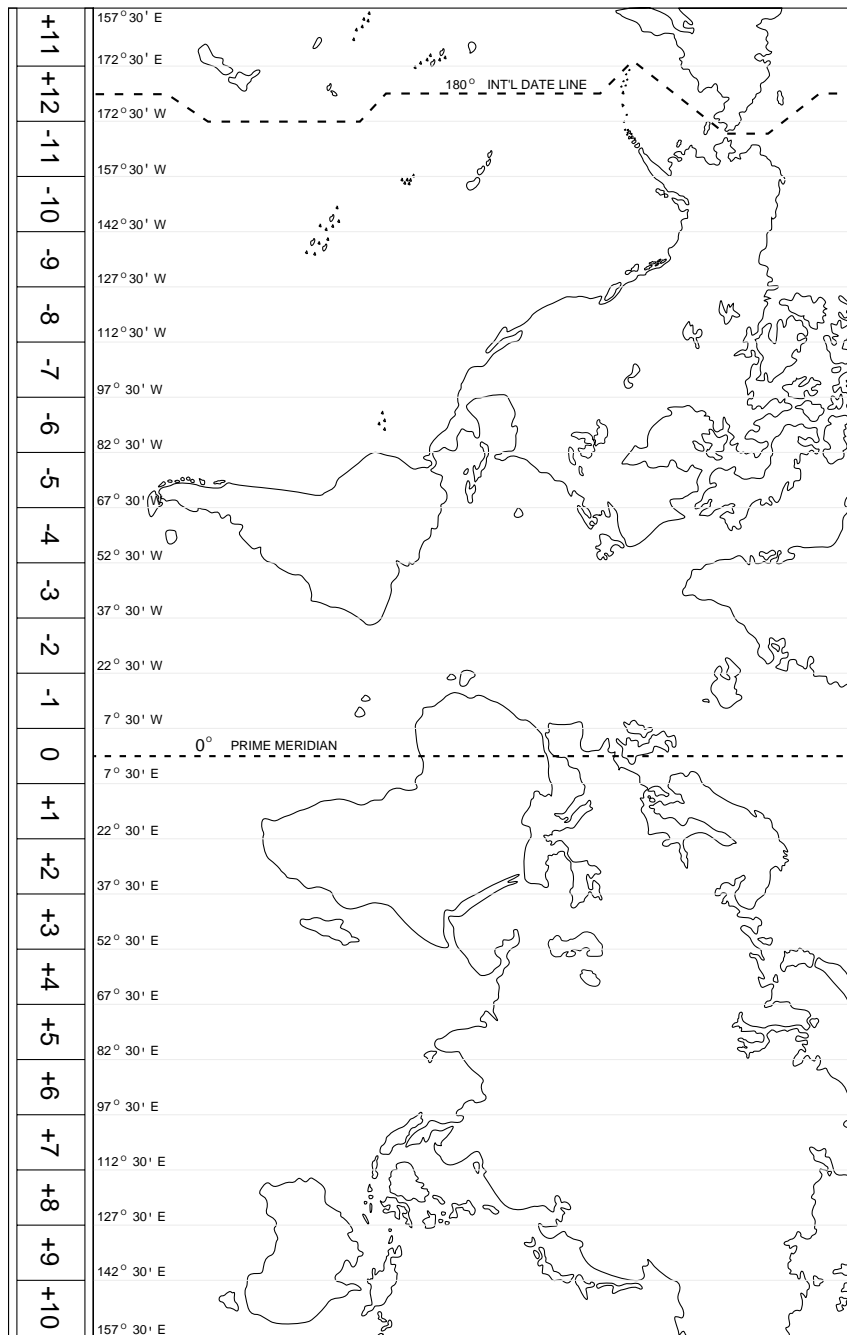
Campbell, G. S. 1977. An Introduction to Environmental Biophysics. Springer Verlag, N. Y. 159 p.

Jensen, M. E., R. D. Burman, and R. G. Allen. 1990. Evapotranspiration and Irrigation Water Requirements. Am. Soc. Civil. Eng. Manual 70, ASCE, 345 E. 47th St., New York, NY 10017-2398

Monteith, J. L. and M. H. Unsworth. 1990. Principles of Environmental Physics, 2nd Ed., Edward Arnold, London. 289 p.

Smith, M. 1991. Report on the expert consultation on procedures for revision of FAO guidelines for prediction of crop water requirements. Food and Agriculture Organization of the United Nations, Rome, Italy.

Allen, R. G., M. E. Jensen, J. L. Wright, and R. D. Burman. 1989. Operational estimates of reference evapotranspiration. Agron. J. 81(4):650-662.



**FIGURE 1. Time Zones**

```

;{CR10X}
;
;Program: MetData 1 weather station program that calculates
;hourly Penman-Monteith Potential Evapotranspiration (ETo).
;
;Date: 15.June.1998
;
;*B CR10X STATUS/ON-BOARD FIRMWARE WITH PRO-
GRAM LOADED
;-----
;01: 18927
;02: 26114
;03: 0256
;04: 00
;05: 00
;06: 1.0000
;07: 0007
;08: 3.152.0
;09: 00
;10: 00
;11: 0.0000
;
;INPUT CHANNEL USAGE
;-----
;S.E. CHANNEL 1 - Relative Humidity (HMP45C)
;S.E. CHANNEL 2 - Air Temperature (HMP45C)
;S.E. CHANNEL 3 - Wind Direction (034A)
;DIFF CHANNEL 3 - Pyranometer (LI200X)
;S.E. CHANNEL 10 - Enclosure Relative Humidity
;
;EXCITATION CHANNEL USAGE
;-----
;E2 - Wind Direction (034A)
;
;PULSE CHANNEL USAGE
;-----
;P1 - Wind Speed (034A)
;P2 - Tipping Rain Bucket (TE525)
;
;CONTROL PORT USAGE
;-----
;C1 - Relative Humidity and Air Temperature (HMP45C)
;
;FINAL STORAGE DATA ARRAY DEFINITIONS
;=====
```

;HOURLY DATA

;-----

;1 Array ID - 129  
;2 Year  
;3 Julian Day  
;4 Hour,Minute (HHMM; Midnight = 2400 hours)  
;5 Average Air Temp - °C  
;6 Sample Relative Humidity - %RH  
;7 Average Vapor Pressure - KPa  
;8 Average Solar Flux Density - KW/m<sup>2</sup>  
;9 Hourly ETo Total - inch/hour  
;10 Average Wind Speed - miles/hour  
;11 Average Vector Wind Direction - degrees  
;12 Standard deviation of Wind Direction  
;13 Total Precipitation - inches/hour

;

;DAILY DATA (@MIDNIGHT)

;-----

;1 Array ID - 139  
;2 Year  
;3 Julian Day  
;4 Hour,Minute (HHMM; Midnight = 2400 hours)  
;5 Average Air Temp - °F  
;6 Maximum Air Temp - °F  
;7 Minimum Air Temp - °F  
;8 Average Vapor Pressure - KPa  
;9 Maximum Vapor Pressure - KPa  
;10 Minimum Vapor Pressure - KPa  
;11 Average Solar Flux Density - KW/m<sup>2</sup>  
;12 Daily ETo Total - inches/day  
;13 Maximum Wind Speed - miles/hour  
;14 Average Wind Speed - miles/hour  
;15 Total Precipitation - inches/day  
;16 Maximum Battery Voltage - DC Volts  
;17 Minimum Battery Voltage - DC Volts  
;18 Maximum Datalogger Temp (CR10X) - °C  
;19 Minimum Datalogger Temp (CR10X) - °C  
;20 Maximum Enclosure Relative Humidity - %RH  
;21 Minimum Enclosure Relative Humidity - %RH  
;22 Program Signature

\*Table 1 Program

01: 10.0000 Execution Interval (seconds)

01: Batt Voltage (P10)  
1: 1 Loc [ Batt\_Volt ]

02: Internal Temperature (P17)  
1: 2 Loc [ CR10Tmp\_C ]

03: Do (P86)  
1: 41 Set Port 1 High

04: Excitation with Delay (P22)  
1: 1 Ex Channel  
2: 0 Delay W/Ex (units = 0.01 sec)  
3: 15 Delay After Ex (units = 0.01 sec)  
4: 0 mV Excitation

05: Volt (SE) (P1)  
1: 1 Reps  
2: 25 2500 mV 60 Hz Rejection Range  
3: 2 SE Channel  
4: 3 Loc [ AirTemp\_C ]  
5: .1 Mult  
6: -40 Offset

06: Z=X\*F (P37)  
1: 3 X Loc [ AirTemp\_C ]  
2: 1.8 F  
3: 4 Z Loc [ AirTemp\_F ]

07: Z=X+F (P34)  
1: 4 X Loc [ AirTemp\_F ]  
2: 32 F  
3: 4 Z Loc [ AirTemp\_F ]

08: Volt (SE) (P1)  
1: 1 Reps  
2: 25 2500 mV 60 Hz Rejection Range  
3: 1 SE Channel Record  
4: 5 Loc [ RH ] humidity as a  
5: .001 Mult fraction.  
6: 0 Offset

09: Do (P86)  
1: 51 Set Port 1 Low

10: If (X<=>F) (P89)  
1: 5 X Loc [ RH ]  
2: 3 >=  
3: 1 F  
4: 30 Then Do

11: If (X<=>F) (P89)  
1: 5 X Loc [ RH ]  
2: 4 <  
3: 1.09 F  
4: 30 Then Do

12: Z=F (P30)  
1: 1 F  
2: 0 Exponent of 10  
3: 5 Z Loc [ RH ]

13: End (P95)

14: End (P95)

15: Saturation Vapor Pressure (P56)  
1: 3 Temperature Loc [ AirTemp\_C ]  
2: 35 Loc [ Sat\_VP ]

16: Z=X\*Y (P36)  
1: 35 X Loc [ Sat\_VP ]  
2: 5 Y Loc [ RH ]  
3: 34 Z Loc [ VP\_kPa ]

17: Z=X\*F (P37)  
1: 5 X Loc [ RH ]  
2: 100 F  
3: 5 Z Loc [ RH ]

18: Z=X-Y (P35)  
1: 35 X Loc [ Sat\_VP ]  
2: 34 Y Loc [ VP\_kPa ]  
3: 36 Z Loc [ VPD\_kPa ]

19: Volt (Diff) (P2)

1: 1 Reps  
2: 22 7.5 mV 60 Hz Rejection Range  
3: 3 DIFF Channel  
4: 6 Loc [ Slr\_kWm2 ]  
5: .2 Mult  
6: 0 Offset

20: If (X<=>F) (P89)

1: 6 X Loc [ Slr\_kWm2 ]  
2: 4 <  
3: 0 F  
4: 30 Then Do

21: Z=F (P30)

1: 0 F  
2: 0 Exponent of 10  
3: 6 Z Loc [ Slr\_kWm2 ]

22: End (P95)

23: Pulse (P3)

1: 1 Reps  
2: 1 Pulse Channel 1  
3: 22 Switch Closure, Output Hz  
4: 41 Loc [ WS\_ms ]  
5: .799 Mult  
6: .2811 Offset

24: Z=X\*F (P37)

1: 41 X Loc [ WS\_ms ]  
2: 2.237 F  
3: 7 Z Loc [ WS\_mph ]

25: Excite-Delay (SE) (P4)

1: 1 Reps  
2: 5 2500 mV Slow Range  
3: 3 SE Channel  
4: 2 Excite all reps w/Exchan 2  
5: 2 Delay (units 0.01 sec)  
6: 2500 mV Excitation  
7: 8 Loc [ Wind\_Dir ]  
8: 0.288 Mult  
9: 0 Offset

26: If (X<=>F) (P89)

1: 8 X Loc [ Wind\_Dir ]  
2: 3 >=  
3: 360 F  
4: 30 Then Do

27: Z=X+F (P34)

1: 8 X Loc [ Wind\_Dir ]  
2: -360 F  
3: 8 Z Loc [ Wind\_Dir ]

28: End (P95)

29: Pulse (P3)

1: 1 Reps  
2: 2 Pulse Channel 2  
3: 2 Switch Closure, All Counts  
4: 9 Loc [ Rain\_inch ]  
5: .01 Mult  
6: 0 Offset

30: Volt (SE) (P1)

1: 1 Reps  
2: 25 2500 mV 60 Hz Rejection Range  
3: 10 SE Channel  
4: 28 Loc [ Encl\_RH ]  
5: .1 Mult  
6: 0 Offset

; Compute hourly averages of solar radiation, air temperature,  
; vapor pressure deficit, and wind speed to be used with the ET<sub>o</sub>  
; algorithm. Values go into input locations 37-40.

31: If time is (P92)

1: 0 Minutes (Seconds --) into a  
2: 60 Interval (same units as above)  
3: 10 Set Output Flag High (Flag 0)

32: Set Active Storage Area (P80)

1: 3 Input Storage Area  
2: 37 Loc [ St\_kW\_m2 ]

33: Average (P71)

1: 1 Reps  
2: 6 Loc [ Slr\_kWm2 ]

```

34: Average (P71)
    1: 1      Reps
    2: 3      Loc [ AirTemp_C ]

35: Average (P71)
    1: 1      Reps
    2: 36     Loc [ VPD_kPa  ]

36: Average (P71)
    1: 1      Reps
    2: 41     Loc [ WS_ms   ]

37: If Flag/Port (P91)
    1: 10     Do if Output Flag is High (Flag 0)
    2: 30     Then Do

; Call the ETo algorithm.

38: Do (P86)
    1: 1      Call Subroutine 1

39: End (P95)

40: If time is (P92)
    1: 0      Minutes (Seconds --) into a      Sum up hourly
    2: 60     Interval (same units as above)  ETo and rainfall
    3: 30     Then Do                          values.

41: Z=X+Y (P33)
    1: 26     X Loc [ Rn_Today ]
    2: 11     Y Loc [ HrRainTtl ]
    3: 26     Z Loc [ Rn_Today ]

42: Z=F (P30)
    1: 0      F
    2: 0      Exponent of 10
    3: 11     Z Loc [ HrRainTtl ]

43: Z=X+Y (P33)
    1: 24     X Loc [ ETo_Today ]
    2: 64     Y Loc [ ETo_in_hr ]
    3: 24     Z Loc [ ETo_Today ]

44: End (P95)

```

- 45: Z=X+Y (P33)  
 1: 11 X Loc [ HrRainTtl ]  
 2: 9 Y Loc [ Rain\_inch ]  
 3: 11 Z Loc [ HrRainTtl ]
- 46: If time is (P92) Collect hourly  
 1: 0 Minutes (Seconds --) into a Final Storage  
 2: 60 Interval (same units as above) data.  
 3: 10 Set Output Flag High (Flag 0)
- 47: Set Active Storage Area (P80)  
 1: 1 Final Storage Area 1  
 2: 129 Array ID
- 48: Real Time (P77)  
 1: 1220 Year,Day,Hour/Minute (midnight = 2400)
- 49: Average (P71)  
 1: 1 Reps  
 2: 4 Loc [ AirTemp\_F ]
- 50: Sample (P70)  
 1: 1 Reps  
 2: 5 Loc [ RH ]
- 51: Average (P71)  
 1: 1 Reps  
 2: 34 Loc [ VP\_kPa ]
- 52: Average (P71)  
 1: 1 Reps  
 2: 6 Loc [ Slr\_kWm2 ]
- 53: Sample (P70) Collect ET<sub>o</sub>  
 1: 1 Reps in inches/hour.  
 2: 64 Loc [ ET<sub>o</sub>\_in\_hr ]
- 54: Wind Vector (P69)  
 1: 1 Reps  
 2: 0 Samples per Sub-Interval  
 3: 0 S,  $\theta\lambda$ , &  $\sigma(\theta\lambda)$   
 4: 7 Wind Speed/East Loc [ WS\_mph ]  
 5: 8 Wind Direction/North Loc [ Wind\_Dir ]

55: Totalize (P72)

1: 1 Reps  
2: 9 Loc [ Rain\_inch ]

56: If time is (P92)

1: 0 Minutes (Seconds --) into a  
2: 1440 Interval (same units as above)  
3: 30 Then Do

Move daily ET<sub>o</sub>  
and rainfall  
values. Set  
daily running  
totals back to  
zero.

57: Z=X (P31)

1: 24 X Loc [ ETo\_Today ]  
2: 23 Z Loc [ ETo\_24hr ]

58: Z=F (P30)

1: 0 F  
2: 0 Exponent of 10  
3: 24 Z Loc [ ETo\_Today ]

59: Z=X (P31)

1: 26 X Loc [ Rn\_Today ]  
2: 25 Z Loc [ Rain24hr ]

60: Z=F (P30)

1: 0 F  
2: 0 Exponent of 10  
3: 26 Z Loc [ Rn\_Today ]

61: End (P95)

62: If time is (P92)

1: 0 Minutes (Seconds --) into a  
2: 1440 Interval (same units as above)  
3: 10 Set Output Flag High (Flag 0)

63: Set Active Storage Area (P80)

1: 3 Input Storage Area  
2: 12 Loc [ 24HMxTmpF ]

64: Maximum (P73)

1: 1 Reps  
2: 0 Value Only  
3: 4 Loc [ AirTemp\_F ]

65: Minimum (P74)

1: 1 Reps  
2: 0 Value Only  
3: 4 Loc [ AirTemp\_F ]

66: Average (P71)

1: 1 Reps  
2: 4 Loc [ AirTemp\_F ]

67: Maximum (P73)

1: 1 Reps  
2: 0 Value Only  
3: 5 Loc [ RH ]

68: Minimum (P74)

1: 1 Reps  
2: 0 Value Only  
3: 5 Loc [ RH ]

69: Maximum (P73)

1: 1 Reps  
2: 0 Value Only  
3: 7 Loc [ WS\_mph ]

70: If time is (P92)

1: 0 Minutes (Seconds --) into a Collect daily  
2: 1440 Interval (same units as above) Final Storage  
3: 10 Set Output Flag High (Flag 0) values at  
midnight.

71: Set Active Storage Area (P80)

1: 1 Final Storage Area 1  
2: 139 Array ID

72: Real Time (P77)

1: 1220 Year,Day,Hour/Minute (midnight = 2400)

73: Average (P71)

1: 1 Reps  
2: 4 Loc [ AirTemp\_F ]

74: Maximum (P73)

1: 1 Reps  
2: 0 Value Only  
3: 4 Loc [ AirTemp\_F ]

75: Minimum (P74)

1: 1 Reps  
2: 0 Value Only  
3: 4 Loc [ AirTemp\_F ]

76: Average (P71)

1: 1 Reps  
2: 34 Loc [ VP\_kPa ]

77: Maximum (P73)

1: 1 Reps  
2: 0 Value Only  
3: 34 Loc [ VP\_kPa ]

78: Minimum (P74)

1: 1 Reps  
2: 0 Value Only  
3: 34 Loc [ VP\_kPa ]

79: Average (P71)

1: 1 Reps  
2: 6 Loc [ Slr\_kWm2 ]

80: Sample (P70)

1: 1 Reps  
2: 23 Loc [ ETo\_24hr ]

Collect daily  
ET<sub>o</sub> in  
inches/day.

81: Maximum (P73)

1: 1 Reps  
2: 0 Value Only  
3: 7 Loc [ WS\_mph ]

82: Average (P71)

1: 1 Reps  
2: 7 Loc [ WS\_mph ]

83: Totalize (P72)

1: 1 Reps  
2: 9 Loc [ Rain\_inch ]

84: Maximum (P73)

1: 1 Reps  
2: 0 Value Only  
3: 1 Loc [ Batt\_Volt ]

85: Minimum (P74)

1: 1 Reps  
2: 0 Value Only  
3: 1 Loc [ Batt\_Volt ]

86: Maximum (P73)

1: 1 Reps  
2: 0 Value Only  
3: 2 Loc [ CR10Tmp\_C ]

87: Minimum (P74)

1: 1 Reps  
2: 0 Value Only  
3: 2 Loc [ CR10Tmp\_C ]

88: Maximum (P73)

1: 1 Reps  
2: 0 Value Only  
3: 28 Loc [ Encl\_RH ]

89: Minimum (P74)

1: 1 Reps  
2: 0 Value Only  
3: 28 Loc [ Encl\_RH ]

90: If Flag/Port (P91)

1: 10 Do if Output Flag is High (Flag 0)  
2: 30 Then Do

91: Signature (P19)

1: 27 Loc [ Signature ]

92: End (P95)

93: Sample (P70)

1: 1 Reps  
2: 27 Loc [ Signature ]

94: Serial Out (P96)

1: 71 SM192/SM716/CSM1

\*Table 2 Program

01: 0.0000 Execution Interval (seconds)

\*Table 3 Subroutines

01: Beginning of Subroutine (P85)		Compute ET <sub>o</sub> using Penman-Monteith equation.
1:	1 Subroutine 1	
02: Z=F (P30)		Enter site latitude in degrees.
1:	41.78 F	
2:	0 Exponent of 10	
3:	47 Z Loc [ latitude ]	
03: Z=F (P30)		Enter site longitudinal correction (see equation 11).
1:	-.45667 F	
2:	0 Exponent of 10	
3:	48 Z Loc [ lngt_cor ]	
04: Z=F (P30)		Enter site elevation in feet above sea level.
1:	4454 F	
2:	0 Exponent of 10	
3:	49 Z Loc [ elev_ft ]	
05: Time (P18)		
1:	2 Hours into current year {maximum 8784}	
2:	0 Mod/By	
3:	42 Loc [ clndr_day ]	
06: Z=X*F (P37)		Convert hours to days.
1:	42 X Loc [ clndr_day ]	
2:	.04167 F	
3:	42 Z Loc [ clndr_day ]	
07: Z=X*F (P37)		Scale days for polynomial.
1:	42 X Loc [ clndr_day ]	
2:	.01 F	
3:	65 Z Loc [ day_100 ]	

08: Polynomial (P55)

1: 1 Reps  
2: 65 X Loc [ day\_100 ]  
3: 43 F(X) Loc [ sindec ]  
4: -.37726 C0  
5: -.10564 C1  
6: 1.2458 C2  
7: -.75478 C3  
8: .13627 C4  
9: -.00572 C5

09: If (X<=>F) (P89)

1: 42 X Loc [ clndr\_day ]  
2: 3 >=  
3: 180 F  
4: 30 Then Do

10: Z=X+F (P34)

1: 65 X Loc [ day\_100 ]  
2: -1.8 F  
3: 66 Z Loc [ eq\_of\_tim ]

11 Polynomial (P55)

1: 1 Reps  
2: 66 X Loc [ eq\_of\_tim ]  
3: 66 F(X) Loc [ eq\_of\_tim ]  
4: -.05039 C0  
5: -.33954 C1  
6: .04084 C2  
7: 1.8928 C3  
8: -1.7619 C4  
9: .4224 C5

Equation of  
time  
polynomial  
for last half  
of the year.

12: Else (P94)

13: Polynomial (P55)

1: 1 Reps  
2: 65 X Loc [ day\_100 ]  
3: 66 F(X) Loc [ eq\_of\_tim ]  
4: -.04056 C0  
5: -.74503 C1  
6: .08823 C2  
7: 2.0516 C3  
8: -1.8111 C4  
9: .42832 C5

Equation of  
time  
polynomial  
for first half  
of the year.

14: End (P95)

15: Z=X\*Y (P36)

1: 43 X Loc [ sindec ]  
2: 43 Y Loc [ sindec ]  
3: 44 Z Loc [ cosdec ]

16: Z=X\*F (P37)

1: 44 X Loc [ cosdec ]  
2: -1 F  
3: 44 Z Loc [ cosdec ]

17: Z=Z+1 (P32)

1: 44 Z Loc [ cosdec ]

18: Z=SQRT(X) (P39)

1: 44 X Loc [ cosdec ]  
2: 44 Z Loc [ cosdec ]

cos d =  
(1-(sin d)<sup>2</sup>)<sup>1/2</sup>

19: Z=SIN(X) (P48)

1: 47 X Loc [ latitude ]  
2: 45 Z Loc [ sind\_sinl ]

20: Z=X\*Y (P36)

1: 43 X Loc [ sindec ]  
2: 45 Y Loc [ sind\_sinl ]  
3: 45 Z Loc [ sind\_sinl ]

Sine of  
latitude.

21: Z=X+F (P34)

1: 47 X Loc [ latitude ]  
2: 90 F  
3: 46 Z Loc [ cosd\_cosl ]

22: Z=SIN(X) (P48)

1: 46 X Loc [ cosd\_cosl ]  
2: 46 Z Loc [ cosd\_cosl ]

Cosine of  
latitude.

23: Z=X\*Y (P36)

1: 44 X Loc [ cosdec ]  
2: 46 Y Loc [ cosd\_cosl ]  
3: 46 Z Loc [ cosd\_cosl ]

- 24: Time (P18)  
 1: 1 Minutes into current day (maximum 1440)  
 2: 0 Mod/By  
 3: 50 Loc [ t\_to ]
- 25:  $Z=X*F$  (P37) Convert to  
 1: 50 X Loc [ t\_to ] hours.  
 2: .01667 F  
 3: 50 Z Loc [ t\_to ]
- 26:  $Z=X+F$  (P34) Subtract an  
 1: 50 X Loc [ t\_to ] extra half  
 2: -12.5 F hour to get  
 3: 50 Z Loc [ t\_to ] the time at the  
 middle of the  
 averaging  
 interval.
- 27:  $Z=X+Y$  (P33)  
 1: 50 X Loc [ t\_to ]  
 2: 48 Y Loc [ lngt\_cor ]  
 3: 50 Z Loc [ t\_to ]
- 28:  $Z=X+Y$  (P33)  
 1: 50 X Loc [ t\_to ]  
 2: 66 Y Loc [ eq\_of\_tim ]  
 3: 50 Z Loc [ t\_to ]
- 29:  $Z=X*F$  (P37) Convert to  
 1: 50 X Loc [ t\_to ] degrees.  
 2: 15 F  
 3: 51 Z Loc [ sin\_elev ]
- 30:  $Z=X+F$  (P34)  
 1: 51 X Loc [ sin\_elev ]  
 2: 90 F  
 3: 51 Z Loc [ sin\_elev ]
- 31:  $Z=\text{SIN}(X)$  (P48)  
 1: 51 X Loc [ sin\_elev ]  
 2: 51 Z Loc [ sin\_elev ]
- 32:  $Z=X*Y$  (P36)  
 1: 51 X Loc [ sin\_elev ]  
 2: 46 Y Loc [ cosd\_cosl ]  
 3: 51 Z Loc [ sin\_elev ]

33: Z=X+Y (P33) sin  $\phi$  =  
 1: 51 X Loc [ sin\_elev ] (sin d) (sin l) +  
 2: 45 Y Loc [ sind\_sinl ] (cos d) (cos l)  
 3: 51 Z Loc [ sin\_elev ] (cos(15x(t-t<sub>0</sub>)))

34: If (X<=>F) (P89)  
 1: 51 X Loc [ sin\_elev ]  
 2: 4 <  
 3: 0 F  
 4: 30 Then Do

35: Z=F (P30)  
 1: 0 F  
 2: 0 Exponent of 10  
 3: 51 Z Loc [ sin\_elev ]

36: End (P95)

37: Z=X\*F (P37) S<sub>0</sub> = 1.36 \* sin  $\phi$   
 1: 51 X Loc [ sin\_elev ]  
 2: 1.36 F  
 3: 52 Z Loc [ So\_kW\_m2 ]

38: If (X<=>F) (P89)  
 1: 51 X Loc [ sin\_elev ]  
 2: 3 >=  
 3: .3 F  
 4: 30 Then Do

39: Z=X/Y (P38)  
 1: 37 X Loc [ St\_kW\_m2 ]  
 2: 52 Y Loc [ So\_kW\_m2 ]  
 3: 53 Z Loc [ funcSt\_So ]

40: If (X<=>F) (P89) Limit range of  
 1: 53 X Loc [ funcSt\_So ] S<sub>f</sub>/S<sub>0</sub> to 0.2-0.8  
 2: 3 >=  
 3: .8 F  
 4: 30 Then Do

41: Z=F (P30)  
 1: .8 F  
 2: 0 Exponent of 10  
 3: 53 Z Loc [ funcSt\_So ]

42: End (P95)

43: If (X<=>F) (P89)

1: 53 X Loc [ funcSt\_So ]  
2: 4 <  
3: .2 F  
4: 30 Then Do

44: Z=F (P30)

1: .2 F  
2: 0 Exponent of 10  
3: 53 Z Loc [ funcSt\_So ]

45: End (P95)

46: Z=X\*F (P37)

1: 53 X Loc [ funcSt\_So ]  
2: 7.9 F  
3: 53 Z Loc [ funcSt\_So ]

47: Z=EXP(X) (P41)

1: 53 X Loc [ funcSt\_So ]  
2: 53 Z Loc [ funcSt\_So ]

48: Z=X\*F (P37)

1: 53 X Loc [ funcSt\_So ]  
2: .034 F  
3: 53 Z Loc [ funcSt\_So ]

49: Z=Z+1 (P32)

1: 53 Z Loc [ funcSt\_So ]

50: Z=1/X (P42)

1: 53 X Loc [ funcSt\_So ]  
2: 53 Z Loc [ funcSt\_So ]

51: Z=X\*F (P37)

1: 53 X Loc [ funcSt\_So ]  
2: -1 F  
3: 53 Z Loc [ funcSt\_So ]

52: Z=X+F (P34)

1: 53 X Loc [ funcSt\_So ]  
2: 1 F  
3: 53 Z Loc [ funcSt\_So ]

Cloud effect  
on isothermal  
long wave.

53: End (P95)	
54: Z=X*F (P37)	
1: 38 X Loc [ AvgTempC ]	
2: .0003 F	
3: 54 Z Loc [ Lni_clear ]	
55: Z=X+F (P34)	Unsworth-Monteith formula:
1: 54 X Loc [ Lni_clear ]	$L_{nic} =$
2: -.107 F	$(0.0003)(T_a) -$
3: 54 Z Loc [ Lni_clear ]	$0.107 \text{ W/m}^2$
56: Z=X*Y (P36)	
1: 53 X Loc [ funcSt_So ]	
2: 54 Y Loc [ Lni_clear ]	
3: 55 Z Loc [ Lni ]	
57: Z=X*F (P37)	Assume reference crop albedo is 0.23, $(a_s)(S_i) = 0.77$
1: 37 X Loc [ St_kW_m2 ]	
2: .77 F	
3: 56 Z Loc [ Rn_G ]	
58: Z=X+Y (P33)	
1: 56 X Loc [ Rn_G ]	
2: 55 Y Loc [ Lni ]	
3: 56 Z Loc [ Rn_G ]	
59: If (X<=>F) (P89)	If $S_i > 10 \text{ W/m}^2$ then $r_c$ is 70 s/m and $G = (0.1)(R_n)$ else set $r_c$ to 700 s/m for night and $G = (0.5)(R_n)$ .
1: 37 X Loc [ St_kW_m2 ]	
2: 3 >=	
3: .01 F	
4: 30 Then Do	
60: Z=X*F (P37)	Assume G is $(0.1)(R_n)$ for reference crop during the day or $(0.5)(R_n)$ at night.
1: 56 X Loc [ Rn_G ]	
2: .9 F	
3: 56 Z Loc [ Rn_G ]	
61: Z=F (P30)	
1: 70 F	
2: 0 Exponent of 10	
3: 57 Z Loc [ rv ]	

62: Else (P94)

63:  $Z=X*F$  (P37)

1: 56 X Loc [ Rn\_G ]  
 2: .5 F  
 3: 56 Z Loc [ Rn\_G ]

64:  $Z=F$  (P30)

1: 700 F  
 2: 0 Exponent of 10  
 3: 57 Z Loc [ rv ]

65: End (P95)

66:  $Z=1/X$  (P42)

1: 40 X Loc [ AvgWS\_ms ]  
 2: 67 Z Loc [ ra ]

67:  $Z=X*F$  (P37)

1: 67 X Loc [ ra ]  
 2: 240 F  
 3: 67 Z Loc [ ra ]

$r_a = 209/u_2$   
 (2 meters) or  
 $240/u_3$   
 (3 meters)

68:  $Z=X+Y$  (P33)

1: 57 X Loc [ rv ]  
 2: 67 Y Loc [ ra ]  
 3: 57 Z Loc [ rv ]

Add boundary  
 layer  
 resistance.

69:  $Z=X*F$  (P37)

1: 49 X Loc [ elev\_ft ]  
 2: .001 F  
 3: 59 Z Loc [ GmmaPrime ]

70:  $Z=X*F$  (P37)

1: 59 X Loc [ GmmaPrime ]  
 2: -.03588 F  
 3: 59 Z Loc [ GmmaPrime ]

71:  $Z=EXP(X)$  (P41)

1: 59 X Loc [ GmmaPrime ]  
 2: 59 Z Loc [ GmmaPrime ]

$P/P_o = \exp$   
 (-altitude(feet)/  
 27870)

72: Z=X*F (P37)	<table style="width: 100%; border-collapse: collapse;"> <tbody> <tr><td style="width: 5%;">1:</td><td style="width: 15%;">59</td><td style="width: 80%;">X Loc [ GmmaPrime ]</td></tr> <tr><td>2:</td><td>67.3</td><td>F</td></tr> <tr><td>3:</td><td>59</td><td>Z Loc [ GmmaPrime ]</td></tr> </tbody> </table>	1:	59	X Loc [ GmmaPrime ]	2:	67.3	F	3:	59	Z Loc [ GmmaPrime ]	$\gamma$ at sea level and 20° Celsius is 67.3 Pa. This multiplies the altitude correction.																		
1:	59	X Loc [ GmmaPrime ]																											
2:	67.3	F																											
3:	59	Z Loc [ GmmaPrime ]																											
73: Z=X*Y (P36)	<table style="width: 100%; border-collapse: collapse;"> <tbody> <tr><td style="width: 5%;">1:</td><td style="width: 15%;">59</td><td style="width: 80%;">X Loc [ GmmaPrime ]</td></tr> <tr><td>2:</td><td>57</td><td>Y Loc [ rv ]</td></tr> <tr><td>3:</td><td>59</td><td>Z Loc [ GmmaPrime ]</td></tr> </tbody> </table>	1:	59	X Loc [ GmmaPrime ]	2:	57	Y Loc [ rv ]	3:	59	Z Loc [ GmmaPrime ]																			
1:	59	X Loc [ GmmaPrime ]																											
2:	57	Y Loc [ rv ]																											
3:	59	Z Loc [ GmmaPrime ]																											
74: Z=X/Y (P38)	<table style="width: 100%; border-collapse: collapse;"> <tbody> <tr><td style="width: 5%;">1:</td><td style="width: 15%;">59</td><td style="width: 80%;">X Loc [ GmmaPrime ]</td></tr> <tr><td>2:</td><td>67</td><td>Y Loc [ ra ]</td></tr> <tr><td>3:</td><td>59</td><td>Z Loc [ GmmaPrime ]</td></tr> </tbody> </table>	1:	59	X Loc [ GmmaPrime ]	2:	67	Y Loc [ ra ]	3:	59	Z Loc [ GmmaPrime ]	$\gamma^* = \gamma^* \cdot r_v / r_a$																		
1:	59	X Loc [ GmmaPrime ]																											
2:	67	Y Loc [ ra ]																											
3:	59	Z Loc [ GmmaPrime ]																											
75: If (X<=>F) (P89)	<table style="width: 100%; border-collapse: collapse;"> <tbody> <tr><td style="width: 5%;">1:</td><td style="width: 15%;">38</td><td style="width: 80%;">X Loc [ AvgTempC ]</td></tr> <tr><td>2:</td><td>4</td><td>&lt;</td></tr> <tr><td>3:</td><td>-5</td><td>F</td></tr> <tr><td>4:</td><td>30</td><td>Then Do</td></tr> </tbody> </table>	1:	38	X Loc [ AvgTempC ]	2:	4	<	3:	-5	F	4:	30	Then Do																
1:	38	X Loc [ AvgTempC ]																											
2:	4	<																											
3:	-5	F																											
4:	30	Then Do																											
76: Z=F (P30)	<table style="width: 100%; border-collapse: collapse;"> <tbody> <tr><td style="width: 5%;">1:</td><td style="width: 15%;">-5</td><td style="width: 80%;">F</td></tr> <tr><td>2:</td><td>0</td><td>Exponent of 10</td></tr> <tr><td>3:</td><td>60</td><td>Z Loc [ delta ]</td></tr> </tbody> </table>	1:	-5	F	2:	0	Exponent of 10	3:	60	Z Loc [ delta ]																			
1:	-5	F																											
2:	0	Exponent of 10																											
3:	60	Z Loc [ delta ]																											
77: Else (P94)																													
78: Z=X (P31)	<table style="width: 100%; border-collapse: collapse;"> <tbody> <tr><td style="width: 5%;">1:</td><td style="width: 15%;">38</td><td style="width: 80%;">X Loc [ AvgTempC ]</td></tr> <tr><td>2:</td><td>60</td><td>Z Loc [ delta ]</td></tr> </tbody> </table>	1:	38	X Loc [ AvgTempC ]	2:	60	Z Loc [ delta ]																						
1:	38	X Loc [ AvgTempC ]																											
2:	60	Z Loc [ delta ]																											
79: End (P95)																													
80: Polynomial (P55)	<table style="width: 100%; border-collapse: collapse;"> <tbody> <tr><td style="width: 5%;">1:</td><td style="width: 15%;">1</td><td style="width: 80%;">Reps</td></tr> <tr><td>2:</td><td>60</td><td>X Loc [ delta ]</td></tr> <tr><td>3:</td><td>60</td><td>F(X) Loc [ delta ]</td></tr> <tr><td>4:</td><td>45.3</td><td>C0</td></tr> <tr><td>5:</td><td>2.97</td><td>C1</td></tr> <tr><td>6:</td><td>.0549</td><td>C2</td></tr> <tr><td>7:</td><td>.00223</td><td>C3</td></tr> <tr><td>8:</td><td>0</td><td>C4</td></tr> <tr><td>9:</td><td>0</td><td>C5</td></tr> </tbody> </table>	1:	1	Reps	2:	60	X Loc [ delta ]	3:	60	F(X) Loc [ delta ]	4:	45.3	C0	5:	2.97	C1	6:	.0549	C2	7:	.00223	C3	8:	0	C4	9:	0	C5	Calculate $\Delta$ by using a polynomial. Result is Pa/°C.
1:	1	Reps																											
2:	60	X Loc [ delta ]																											
3:	60	F(X) Loc [ delta ]																											
4:	45.3	C0																											
5:	2.97	C1																											
6:	.0549	C2																											
7:	.00223	C3																											
8:	0	C4																											
9:	0	C5																											

81:  $Z=X+Y$  (P33)

1: 60 X Loc [ delta ]  
2: 59 Y Loc [ GmmaPrime ]  
3: 61 Z Loc [ Erad\_mm\_h ]

82:  $Z=X/Y$  (P38)

$\gamma^*/(\Delta + \gamma^*)$

1: 59 X Loc [ GmmaPrime ]  
2: 61 Y Loc [ Erad\_mm\_h ]  
3: 62 Z Loc [ Eaer\_mm\_h ]

83:  $Z=X/Y$  (P38)

$\Delta/(\Delta + \gamma^*)$

1: 60 X Loc [ delta ]  
2: 61 Y Loc [ Erad\_mm\_h ]  
3: 61 Z Loc [ Erad\_mm\_h ]

84:  $Z=X*Y$  (P36)

1: 61 X Loc [ Erad\_mm\_h ]  
2: 56 Y Loc [ Rn\_G ]  
3: 61 Z Loc [ Erad\_mm\_h ]

85:  $Z=X*F$  (P37)

1: 61 X Loc [ Erad\_mm\_h ]  
2: 1.47 F  
3: 61 Z Loc [ Erad\_mm\_h ]

86:  $Z=X*F$  (P37)

Convert to  
mm/hr.

1: 62 X Loc [ Eaer\_mm\_h ]  
2: 26.6 F  
3: 62 Z Loc [ Eaer\_mm\_h ]

87:  $Z=X*Y$  (P36)

1: 62 X Loc [ Eaer\_mm\_h ]  
2: 39 Y Loc [ Avg\_VPD ]  
3: 62 Z Loc [ Eaer\_mm\_h ]

88:  $Z=X/Y$  (P38)

1: 62 X Loc [ Eaer\_mm\_h ]  
2: 57 Y Loc [ rv ]  
3: 62 Z Loc [ Eaer\_mm\_h ]

89:  $Z=X+Y$  (P33)

1: 61 X Loc [ Erad\_mm\_h ]  
2: 62 Y Loc [ Eaer\_mm\_h ]  
3: 63 Z Loc [ ETo\_mm\_hr ]

90: If (X<=>F) (P89)

```

1:   63      X Loc [ ETo_mm_hr ]
2:   4       <
3:   0       F
4:   30      Then Do
    
```

91: Z=F (P30)

```

1:   0       F
2:   0       Exponent of 10
3:   63      Z Loc [ ETo_mm_hr ]
    
```

ET<sub>o</sub> must be  
> = 0.

92: End (P95)

93: Z=X\*F (P37)

```

1:   63      X Loc [ ETo_mm_hr ]
2:   .03937 F
3:   64      Z Loc [ ETo_in_hr ]
    
```

Converts ET<sub>o</sub>  
mm/hr to  
inches/hr.

94: End (P95)

End Program

-Input Locations-

```

1 Batt_Volt
2 CR10Tmp_C
3 AirTemp_C
4 AirTemp_F
5 RH
6 Slr_kWm2
7 WS_mph
8 Wind_Dir
9 Rain_inch
10 _____
11 HrRainTtl
12 24HMxTmpF
13 24HMnTmpF
14 24HAvtmpF
15 24HMaxRH
16 24HMinRH
17 24HMaxWS
18 _____
19 _____
20 _____
21 _____
22 _____
    
```

23 ETo\_24hr  
24 ETo\_Today  
25 Rain24hr  
26 Rn\_Today  
27 Signature  
28 Encl\_RH  
29 \_\_\_\_\_  
30 \_\_\_\_\_  
31 \_\_\_\_\_  
32 \_\_\_\_\_  
33 \_\_\_\_\_  
34 VP\_kPa  
35 Sat\_VP  
36 VPD\_kPa  
37 St\_kW\_m2  
38 AvgTempC  
39 Avg\_VPD  
40 AvgWS\_ms  
41 WS\_ms  
42 clndr\_day  
43 sindec  
44 cosdec  
45 sind\_sinl  
46 cosd\_cosl  
47 latitude  
48 lngt\_cor  
49 elev\_ft  
50 t\_to  
51 sin\_elev  
52 So\_kW\_m2  
53 funcSt\_So  
54 Lni\_clear  
55 Lni  
56 Rn\_G  
57 rv  
58 \_\_\_\_\_  
59 GmmaPrime  
60 delta  
61 Erad\_mm\_h  
62 Eaer\_mm\_h  
63 ETo\_mm\_hr  
64 ETo\_in\_hr  
65 day\_100  
66 eq\_of\_tim  
67 ra

68 \_\_\_\_\_  
69 \_\_\_\_\_  
70 \_\_\_\_\_  
129 \_\_\_\_\_ 0 0 0  
139 \_\_\_\_\_ 0 0 0  
-Program Security-  
0000  
0000  
0000  
-Mode 4-  
-Final Storage Area 2-  
0  
-CR10X ID-  
0  
-CR10X Power Up-  
3